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No. CBS/DRO Dated: 31-08-2020

#### **Chief Bridge Engineer:**

- 1. Central Railway, Mumbai CST-400 001.
- 2. Eastern Railway, Fairlie Place, Kolkata-700 001.
- 3. East Central Railway, Hazipur-844 101.
- 4. East-Coast Railway, Bhubaneshwar-751 016 (Orissa).
- 5. Northern Railway, Baroda House, New Delhi- 110 001.
- North-Central Railway, Allahabad-211 001.
- 7. North Eastern Railway, Gorakhpur-273 001.
- 9. Northeast Frontier Railway, Maligaon, Guwahati-781 011.
- 10. Southern Railway, Park Town, Chennai-600 003.
- 11. South Central Railway, Rail Nilayam, Secunderabad-500 371.
- 12. South East Central Railway, Bilaspur-495 004
- 13. South Eastern Railway, Garden Reach, Kolkata-700 043
- 14. South-West Railway, Hubli-580 023.
- 15. Western Railway, Mumbai-400 020.
- 16. West-Central Railway, Jabalpur-482 001.

**Sub:** Checking of Non-Standard Composite Girder ROBs.

- Ref: 1. Railway Board letter no. 2015/CE-IV/ROB/78 Pt. dated 23.06.2020.
  - 2. VC of Railway Board with RDSO on 08.07.2020 and 25.08.2020.

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- 1.0 With respect to above subject and vide ref. (1) above, Railway Board has advised Zonal Railways to approve the non-standard girders of NHAI on its own. Moreover vide ref. (2), Railway Board advised RDSO to prepare a guideline for checking of non-standard composite girder ROBs. These guidelines will be issued to Zonal Railways and thereafter no non-standard design of composite girder of ROBs will be considered by RDSO.
- 2.0 Accordingly a guideline in form of checklist of important parameters to be checked during design check of the composite I-Girder has been prepared and is being given as annexure-I of this letter. Although all efforts have been taken to cover the items related to checking of design of composite I-Girder but there

- might be some inadvertent errors or some issues might have not been covered. So any suggestions to improve the guideline are welcome.
- 3.0 In view of Railway Board's advice vide ref. (1) and (2), it is submitted that RDSO will not consider the design of non-standard composite girder henceforth.

This is for your kind information and further necessary action.

DA: Annexure-I (7 Pages)

(Rajesh Kumar Srivastava) ED/B&S/ Steel

#### Copy to:

- I. PED/Bridge/Railway Board, Rail Bhavan, New Delhi-110001 for kind information.
- II. Chief Engineer, Metro Railway, Jawahar Lal Nehru Road, Kolkata-700071 for information and necessary action.

(Rajesh Kumar Srivastava) ED/B&S/ Steel

### Annexure-I

# Checklist for important design checks of I-Girder type composite ROB

S. No.	Description	Check points	
	1.0 General Arrangement of structure		
a.	Effective Span Length	As per GAD.	
b.	Skew	• For planning ROB with lesser skew refer BS-112 (Latest version) guidelines of RDSO.	
		• It is preferable that skew should be limited to 20 degree as far as possible for applicability of square design calculations with certain precautions. However if it not possible due to site conditions then it should be accounted suitably in analysis and design calculations.	
c.	Projection of I-Girder Beyond C/L of bearing	Preferably within 500 mm. beyond centre line of bearing	
d.	Slab overhang beyond steel I-girder	Preferably within 250 mm. beyond girder end	
e.	Overall Length of Girder	As per GAD	
f.	Width of Carriage Way	As per GAD and as per IRC special	
g.	Overall Width of Slab	publication for planning of Highways such as IRC SP 84; IRC SP 87 etc.	
h.	No. of steel girder and C/C spacing of girder	Provisions of IRC Clause 504.3 of IRC:24-2010	
i.	Haunch	• Deck slab with or without haunch to be decided.	
		• Haunch details to be decided as per Cl.606.7 of IRC: 22-2015.	
j.	Footpath	As per GAD or applicable IRC standards.	
	2.0 Material Specification		
a.	Grade of steel	• E350 grade B0 as per IS 2062-2011 should be used preferably over E250 grade B0.	
		• In case of steel of grade higher than E350, issue of weldability of such steel to be checked as RDSO has not done any design in steel greater than E350.	

b.	Grade of Concrete	In deck slab M40 or M45 grade
c.	Grade of reinforcement	Ductile grade reinforcement steel should
		be used. Normally Fe 500 D should be
		used however other grades can be used
		which have ductile grade.
d.	HSFG bolting assemblies	Material specification and other
	with DTI washers	stipulations related to it as per RDSO
		report no. BS 111 (Latest version)
e.	STUD shear connector	IRC 22:2015 and RDSO report no. BS 115
		(Latest version)
	3	3.0 Loading
a.	Dead load	Dead load calculation as per general
		arrangement decided. Unit weights form Cl
		203 of IRC 6:2017.
Ъ.	SIDL	SIDL calculation considering Crash
		barrier, railing, cables, bitumen top,
		wearing coat etc.
c.	Crash Barrier	Clause 109.6 of IRC:5-2015 & Cl 206 of
		IRC:6-2017
d.	Safety Kerb	• Clause 109.8 of IRC:5-2015
		• 400 kg/m2 pedestrian live load
		considered on safety kerb. Cl 206 IRC:6-
		2017
e.	Live Loading	• Cl 204 of IRC:6-2017.
		• To be decided as per width of
		carriageway. Different combination of
		Class A and 70R to be taken as per
		number of lanes in considered in
		carriageway given in Table 6 and 6A of
		IRC:6-2017.
		• Placement of loads along width of
		carriageway as per IRC 6:2017.
f.	Impact factor	From Clause 208.2 & 208.3 of IRC: 6-
	Q ' 1 T/ 1 ' 1 (QT/)	2017
g.	Special Vehicle (SV)	Applicability to be confirmed from
	loading	concerned road authorities and girder to
		be checked for SV loading in case this
		loading is applicable as per details of Cl
L	Congestion factor	204.5 of IRC:6-2017.
h. i.	Congestion factor Pedestrian loads	As per clause 204.4 of IRC:6-2017
1.	redestrian loads	450 kg/m <sup>2</sup> pedestrian live load considered
2	Contribugal force	on footpath. Cl 206 IRC:6-2017
j. 1-	Centrifugal force	Clause 212 of IRC:6-2017
k.	Longitudinal loads	Clause 208 and 211 of IRC:6-2017
1.	Temperature effect i.e.	Clause 215 of IRC:6-2017

		rise, fall and differential	
		shrinkage	
	m.	Wind load	Clause 209 of IRC:6-2017
	n.	~	Clause 219 of IRC:6-2017
	ο.	Fatigue load	Clause 204.6 of IRC:6-2017
	p.	Load combinations for	
	•	serviceability, ultimate	2017
		and construction stage	
		<u> </u>	in girder section
a.		Proportioning of Main	
		Girder	
		Overall depth of steel	Cl 504.4 of IRC:24-2010
		beam	
		Minimum sections	Cl 504.7 of IRC:24-2010
		Top flange plate	Check classification of section as per table
			2 of IRC 22: 2015.
		Bottom flange plate	Check classification of section as per table
			2 of IRC 22:2015
		Web Plates	Check classification of section as per table
			2 of IRC 22:2015
	_	Effective width of concrete	Cl 603.2 of IRC:22-2015
	b.	Cross section properties	
		Modular ratio	• As per clause 604.3 of IRC 22:2015
			• Short term modular ratio for short term
			load effects
			• Long term modular ratio for permanent
	-	0 1 1	or long term load effects
		Sectional properties	Sectional properties such as Ixx, Iyy, C.G.,
		calculation	Aeq, Zst, Zsb, Zct, Zcb etc. should be
			calculated for steel girder only section,
			concrete only section, Composite section with Kc=0.5 and Composite section with
			Kc=1 for calculation of stresses in different
			loading conditions.
	c.	Capacity calculation of	loading conditions.
		main girder	
		Plastic moment of	As per clause 603.3.1 of IRC 22:2015
		resistance	•
		Shear capacity	Plastic shear capacity: Cl. 603.3.3.2 (1) of
			IRC:22-2015 and Shear buckling capacity:
			C1. 603.3.3.2 (2)(a)
		Buckling resistance	During launching and slab construction
		moment (Construction	stage: Cl.I.5 of Annexure I of IRC:22-2015
		stage)	& Clause 509.2.2 of IRC:24-2010
		Permissible bending	During launching, slab construction and

	compressive stress	final stage: Cl 603.3.1 of IRC:22-2015; Cl 509.2, Table 10, 11, 12, 13 and Cl 509.3 IRC:24-2010
	Permissible tensile stress	Cl. 604.3.1(3) of IRC:22-2015 and fatigue analysis to be done separately
	Permissible stress in concrete	Cl. 12.2.1 of IRC:112-2011
d.	Deflection of main girder	separately for:  • Dead load of steel portion of girder;  • SIDL such as Concrete Deck slab, Crash barrier, wearing coat, macadam, shuttering etc.;  • Live load.  • Live load deflection and total deflection limit is to be checked as per Cl. 604.3.2 of IRC:22-2015
e.	Camber	Check total deflection limit as per Cl. 604.3.2 of IRC:22-2015. If total deflection of girder is under limit then no pre camber is required otherwise pre camber is provided to offset the effect of permanent loads
f.	Weld design for I-Girder	<ul> <li>Weld design for different welds in I-Girder to be done considering permissible stress in weld as per Cl 512.4.5.1.1, IRC:24-2010.</li> <li>To be checked for fatigue as per table 5 of IRC 22-2015</li> </ul>
	5.0 Sh	near Stud design
a.	Stud Height	Height of stud as per clause 606.6 of IRC 22-2015
b.	Stud Diameter	Stud dia. as per clause 606.6 of IRC 22-2015.
	Spacing of stud	Spacing of stud as per clause 606.4 and 606.9 of IRC 22-2015. (Spacing of studs along longitudinal direction should be provided less in end and should be more in middle portion)
d.	Projection in slab	Projection in deck slab as per clause 606.6.1 of IRC 22-2015.
e.	Cover over shear connector	<ul> <li>Cover over shear connector as per clause 606.8 of IRC 22:2015</li> <li>Side cover on girder as per clause 606.9 of IRC 22:2015</li> </ul>

f.	Capacity of stud shear	· 1
	connector	IRC:22-2015 and characteristic properties to be taken from Table III.1, IRC:22-2015
~	Detailing of shear	
g.	connector	As per Cr 000.0 or rkc.22-2013.
		iffener of girder
a.		mener of grider
a.	Outstand limit	Clause 509.7.1.2 of IRC:24-2010
	Bearing length	Cl 509.7.1.3 of IRC:24-2010
	Dispersion length	Cl 509.7.1.3 of IRC.24-2010 Cl 509.7.4 of IRC:24-2010
		Cl 509.7.4 of IRC:24-2010
	Bearing capacity of stiffener	CI 509.7.4 01 IRC:24-2010
		Cl 509.7.1.5 of IRC:24-2010
	stiffener	CI 309.7.1.3 01 IRC.24-2010
	Design of Bearing stiffener	Cl 509.7.6 of IRC:24-2010
	Connection of bearing	
	stiffener	C1 309.7.10 01 IRC.24-2010
h	Intermediate Stiffeners	
<b>D.</b>	Outstand limit	Clause 509.7.1.2 of IRC:24-2010
	Spacing of stiffener	Cl 509.7.2.2 of IRC:24-2010
	Check for web thickness	Cl 509.6.1.1 of IRC:24-2010
	requirement	C1 003.0.1.1 01 IKC.2 1 2010
	Check for compression	Cl 509.6.1.2 of IRC:24-2010
	flange buckling	61 663.6.1.2 61 INC.2 1 2616
	requirement	
	Check for unsupported	Clause 509.7.14 (g) of IRC:24-2010
	clear dimension of web	(6)
	panel	
	Moment of inertia	Cl 509.7.2.4 of IRC:24-2010.
	requirement	
	Buckling check on	Cl 603.3.3.2(2) of IRC:22-2015
	intermediate stiffener	
	Weld connection of	Cl 509.7.2.6 of IRC:24-2010
	intermediate stiffener	
	_	ce Joints of girder
a.	Splice location	• Splice at section of maximum B.M. or
		S.F. to be avoided.
		• Location of splice to be chosen
		considering maximum piece length of 13
		m. and preferably symmetrical w.r.t.
		centre of girder.
ъ.	Bolt value of one HSFG	Considering appropriate grade, dia and
	bolt	slip factor for bolt and no slip condition at
		ultimate load.

c.	Top Flange splice	• Top flange splice cover plates area as per
	ask remede skreet	clause no. 509.6.3.3 of IRC24-2010.
		• It is designed to transfer maximum
		stress of ULS condition at top flange.
d.	Web splice	• Cl 509.6.4.2 of IRC:24-2010.
		• The web splice carries a bending Moment
		equal to the total design moment on the
		section multiplied by the ratio of the
		moment of inertia of the web to the
		moment of inertia of the entire section.
		• In addition to this moment, the web
		splice also carries the Design Shear at
		the splice location and the moment due
		to the eccentricity of the shear force
	D d	considering gap between plates 50mm.
e.	Bottom flange splice	Bottom flange splice cover plates area as
		per clause no. 509.6.3.3 of IRC:24-2010
		(Net flange area should be compared)
		• It is designed to transfer maximum
f.	Arrangement of bolts on	stress of ULS condition at bottom flange Size of cover plates in splices also to be
1.	splice and size of cover	
	plates	limits for HSFG bolts as per IRC 24:2010
	1 4	racings and cross frames of I-girder
a.	End Diaphragm	• End diaphragm to be designed for 50% of
		lateral force and for vertical load of total
		dead load and SIDL coming on each
		girder.
		• Design of End diaphragm and it's
		connection to be done to resist these
		loads in bending as well as axial
		compression as per the case using IRC
		24:2010 considering the locations of
		jacking points • Recommended to have web depth
		• Recommended to have web depth between D to 0.75D, where D is depth of
		girder
		<ul><li>Jacking point on end diaphragm should</li></ul>
		have minimum clear distance of 150
1		1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		mm. from end of bottom flange
<b>b.</b>	Bottom Lateral Bracing	mm. from end of bottom flange  • Designed to resist 25% of lateral force
b.	Bottom Lateral Bracing	<ul> <li>mm. from end of bottom flange</li> <li>Designed to resist 25% of lateral force</li> <li>Bottom lateral bracing Design: For Max</li> </ul>
b.	Bottom Lateral Bracing	• Designed to resist 25% of lateral force

		for both axial tension and compression for max. Force coming on member as per
		IRC: 24-2010
c.	Intermediate cross	
	frame	resist 50% of lateral forces. Member and
		connection to be checked for both axial
		tension and compression for max. Force
		coming on member as per IRC: 24-2010
	9.	0 Deck slab
a.	Values of concrete to be	Cl. 6.4 of IRC:112-2011
	taken in design	
b.	Values of reinforcing steel	Cl. 6.2 of IRC:112-2011
	to be taken in design	
c.	Clear cover	Table 14.2 of IRC:112-2011
d.	Depth of deck slab	Cl 6.2.2, 6.4.2.8, table 6.5 and table 14.2
		of IRC 112-2011
e.	Top & bottom	Cl 16.5.1.1, 12.3.3, 15.2.1(2), 18.4.4.2(3),
	reinforcement	16.6.1.1 of IRC:112-2011
f.	Transverse reinforcement	Cl 16.6.1.1 of IRC: 112-2011
g.		Cl 10.3.2.2 of IRC:112-2011
h.	Crack width consideration	Cl 12.3 of IRC:112-2011
i.	<u> </u>	Cl. 14.3 and 14.4 of IRC:112-2011
j.	General detailing	Cl. 15.2 of IRC:112-2011
	requirement of	
	reinforcement steel	
	related to spacing, bond,	
	anchorage etc.	
k.	Detailing requirement	Cl. 16.6 of IRC:112-2011
	related to solid slab	